

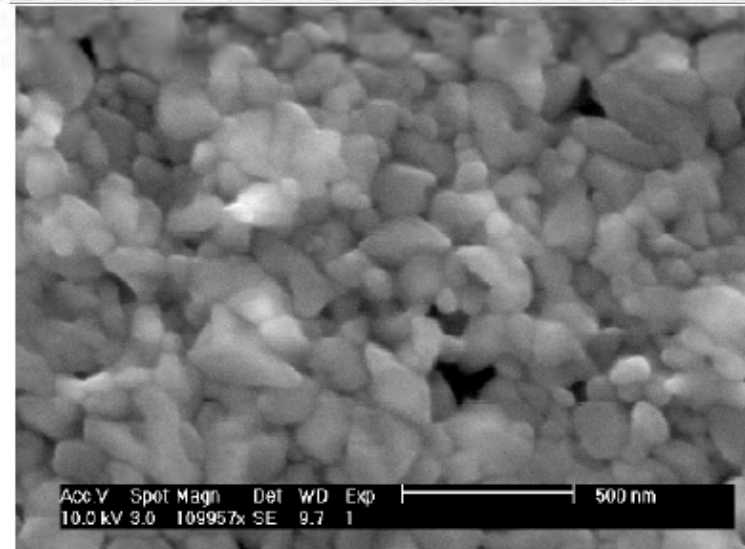
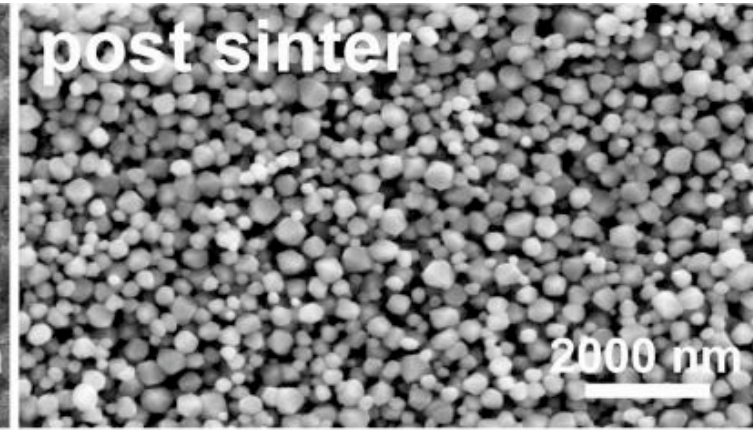
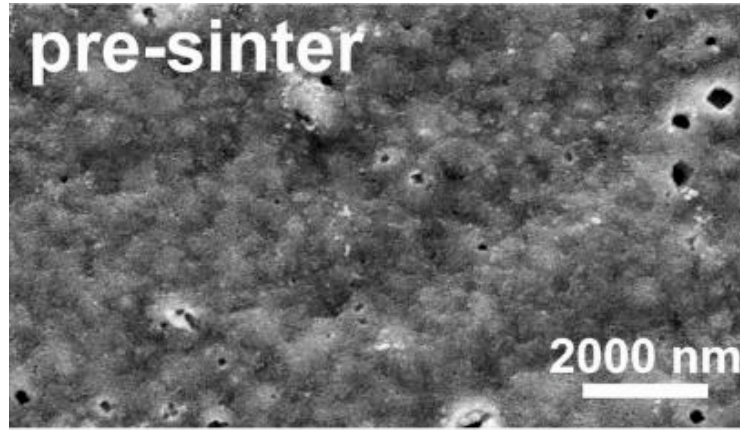
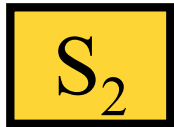


# Sintering Process of Pyrite Nano Particles: A Phase Field Model

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# Motivation





# Motivation

We want to model the sintering process and study the effect of different vapors on the surface energy anisotropy, mobility? and how these anisotropies effect the densification during the annealing?

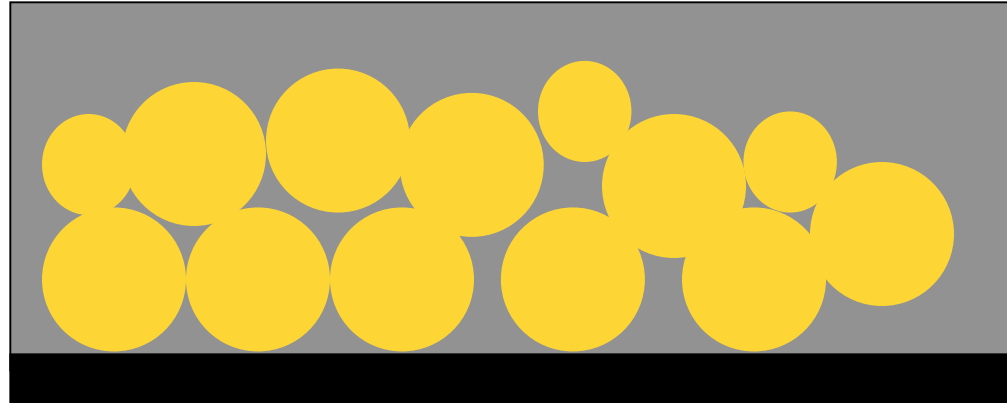


We study the effect of anisotropic surface energy and kinetics on the sintering evolution by diffusive interface phase field models



# Sintering

Vapor



Substrate

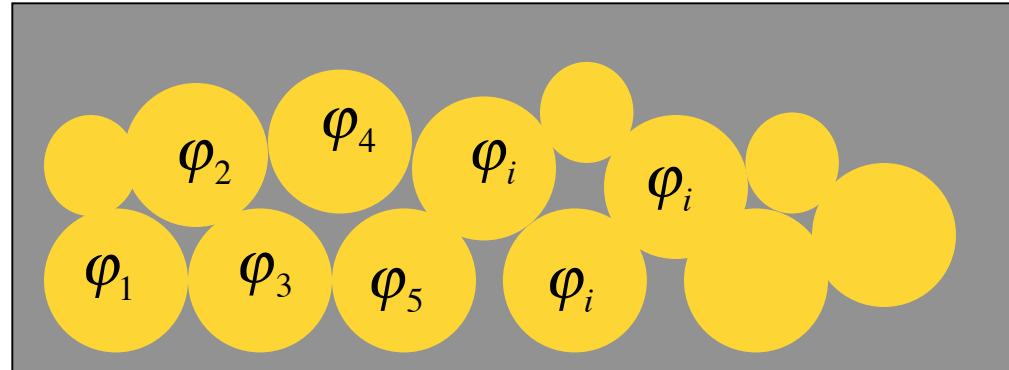
Mass is conserved





# Sintering

Vapor



$$\sum \varphi_i = cte$$





# Phase Field Model

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Vapor

$$\varphi = 0$$

$$\varphi = 1$$



# Classical Diffuse Interface Model

## Cahn-Hilliard system

$$f(\varphi, \nabla \varphi, \nabla^2 \varphi) = f_0 + \sum_i L_i \frac{\partial \varphi}{\partial x_i} + \sum_{ij} \kappa_{ij}^{(1)} \frac{\partial^2 \varphi}{\partial x_i \partial x_j} + \frac{1}{2} \sum_{ij} \kappa_{ij}^{(2)} \frac{\partial \varphi}{\partial x_i} \frac{\partial \varphi}{\partial x_j}$$

$$E(\varphi) = \int_{\Omega} (f_0(\varphi) + \kappa |\nabla \varphi|^2) d\Omega$$

$$f_0 = \varphi^2 (1 - \varphi)^2 / 4 \quad \epsilon^2 = 2\kappa$$

$$\frac{\partial \varphi}{\partial t} = \frac{1}{\epsilon^2} \nabla \cdot (M(\varphi) \nabla \mu)$$

$$\mu = \frac{\partial E}{\partial \varphi} = f_0'(\varphi) - \epsilon^2 \Delta \varphi \quad M(\varphi) = 4\varphi(1 - \varphi) \quad 7$$



# Anisotropic Surface Energy

$$E[\varphi] = \int_{\Omega} \left( f_0 + \frac{\epsilon^2}{2} \Gamma(\mathbf{n}) |\nabla \varphi|^2 \right) d\Omega$$

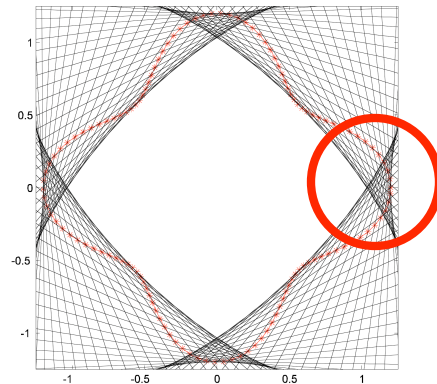
Kobayashi, 1993

$$E[\varphi] = \int_{\Omega} \Gamma(\mathbf{n}) \left( f_0 + \frac{\epsilon^2}{2} |\nabla \varphi|^2 \right) d\Omega$$

Torabi et al., 2009.

$$\Gamma(\mathbf{n}) = 1 + \epsilon_4 \left( 4 \sum_{i=1}^d n_i^4 - 3 \right)$$

$$\Gamma(\theta) = 1 + \epsilon_4 \cos 4\theta$$



ill-posed

$$\Gamma + \Gamma'' < 0$$





# Anisotropic Surface Energy

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Add high order **regularization** term to the **strongly anisotropic energy**

$$\frac{\delta^2}{2} \int_{\Omega} \left( \frac{f_{0'}(\varphi)}{\epsilon^2} - \Delta\varphi \right)^2 d\Omega$$

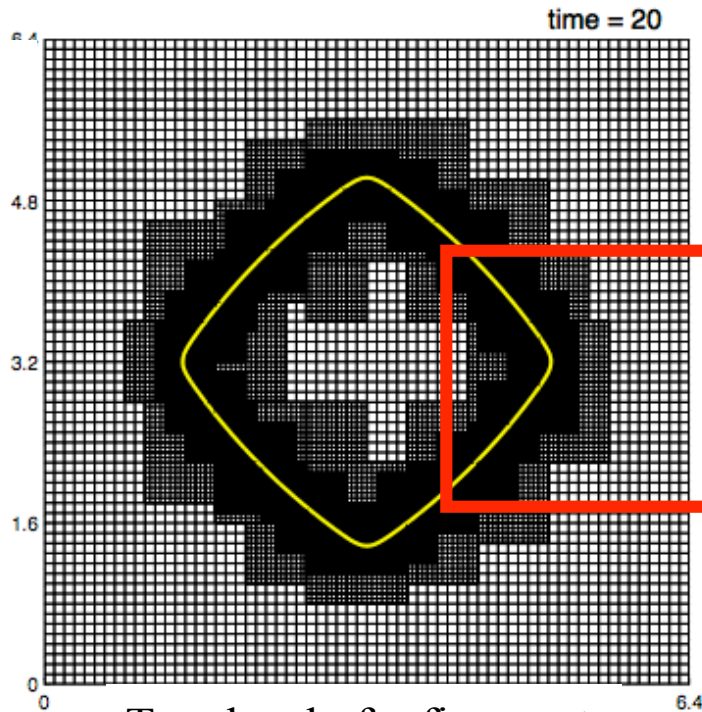
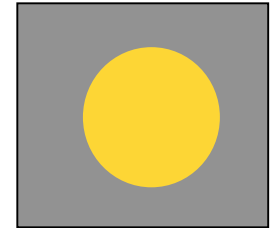
DeGiorgi, 1991;  
Du, Liu, Wang, 2004

$$\frac{\partial\varphi}{\partial t} = \frac{1}{\epsilon^2} \nabla \cdot (M(\varphi) \nabla \mu)$$

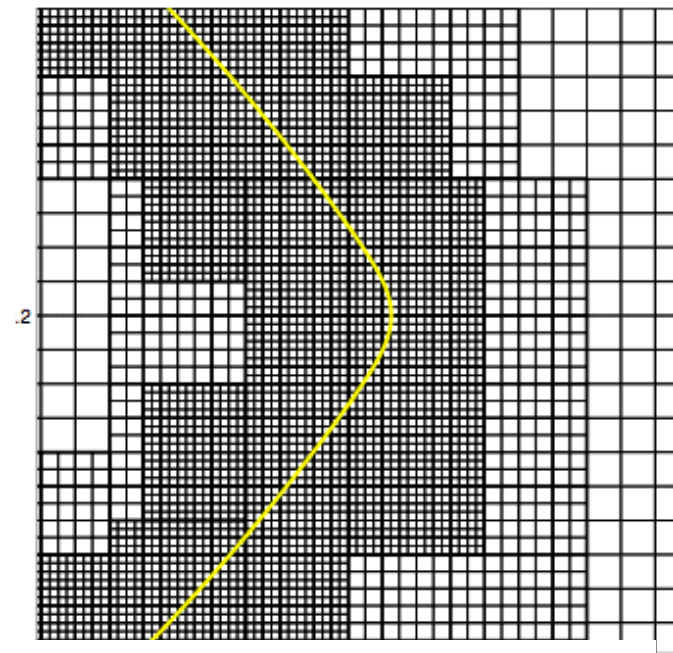


# Numerical Analysis

Adaptive, Nonlinear Multigrid, Finite Difference Method



Two level of refinement.



Finer mesh along the interface

2<sup>nd</sup> order accurate in time and space

Wise, et al, 2007



Is there any **Natural** way to address the anisotropy?



# Extended Cahn-Hilliard Model

## Cubic Symmetry

$$f(\varphi, \nabla \varphi, \nabla^2 \varphi) = f_0 + \frac{1}{2} \sum_{ij} \kappa_{ij} \frac{\partial \varphi}{\partial x_i} \frac{\partial \varphi}{\partial x_j}$$

$$+ \sum_{ijkl} \bar{\gamma}_{ijkl} \frac{\partial^2 \varphi}{\partial x_i \partial x_j} \frac{\partial^2 \varphi}{\partial x_k \partial x_l}$$

Abinandanan et al., 2001

$$+ \sum_{ijkl} \bar{\lambda}_{ijkl} \frac{\partial^2 \varphi}{\partial x_i \partial x_j} \frac{\partial \varphi}{\partial x_k} \frac{\partial \varphi}{\partial x_l} + \sum_{ijkl} \bar{\alpha}_{ijkl} \frac{\partial \varphi}{\partial x_i} \frac{\partial \varphi}{\partial x_j} \frac{\partial \varphi}{\partial x_k} \frac{\partial \varphi}{\partial x_l}$$

$$E(\varphi) = \int_{\Omega} \left( f_0(\varphi) + \kappa |\nabla \varphi|^2 + \bar{\gamma}_{ijkl} \varphi_{ij} \varphi_{kl} + \bar{\lambda}_{ijkl} \varphi_{ij} \varphi_k \varphi_l + \bar{\alpha}_{ijkl} \varphi_i \varphi_j \varphi_k \varphi_l \right) d\Omega$$

$$\varphi_i = \partial \varphi / \partial x_i$$

$$\varphi_{ij} = \partial^2 \varphi / \partial x_i \partial x_j$$



# ECH for Cubic Crystals

$$E(\varphi) = \int_{\Omega} \left( f_0(\varphi) + \frac{\epsilon^2}{2} |\nabla \varphi|^2 \right.$$

$$(\bar{\gamma}, \bar{\lambda}, \bar{\alpha}) \sim \delta^2(\gamma, \lambda, \alpha)$$

$$+ \frac{\delta^2}{2} (\gamma_{11}(\Delta\varphi)^2 + 2(\gamma_{12} - \gamma_{11})\varphi_{11}\varphi_{22} + 4\gamma_{44}\varphi_{12}^2$$

$$+ \lambda_{11} |\nabla \varphi|^2 \Delta\varphi + (\lambda_{12} - \lambda_{11})(\varphi_{11}\varphi_2^2 + \varphi_{22}\varphi_1^2) + 4\lambda_{44}\varphi_{12}\varphi_1\varphi_2$$

$$+ \alpha_{11} |\nabla \varphi|^4 + 2(\alpha_{12} + 2\alpha_{44} - \alpha_{11})\varphi_1^2\varphi_2^2) d\Omega$$

$$\mu = f_0'(\varphi) - \epsilon^2 v + \delta^2 (\gamma_{11} \Delta v + 2(\gamma_{12} + 2\gamma_{44} - \gamma_{11})\omega_{12}$$

$$+ 2(\lambda_{44} - \lambda_{12})(\varphi_{11}\varphi_{22} - \omega^2)$$

$$- 6\alpha_{11}(\varphi_1^2\varphi_{11} + \varphi_2^2\varphi_2) - 2(\alpha_{12} + 2\alpha_{44})(\varphi_1^2\varphi_{22} + \varphi_2^2\varphi_{11} + 4\varphi_1\varphi_2\varphi_{12}))$$

$$v = \Delta\varphi, \quad \omega_{12} = \partial^2 \omega / \partial x_1 \partial x_2, \quad \omega = \varphi_{12} = \partial^2 \varphi / \partial x_1 \partial x_2$$



# ECH Model

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- The biggest advantage is having **well posed** model and **no need to regularize the energy**.
- The model can be used in **energy stable schemes: Energy splits** into purely convex and concave pieces.
- The energy is always **non-increasing in time, regardless of the time step size**

$$E(\varphi^{n+1}) \leq E(\varphi^n)$$



# Energy Stable Scheme

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$$E_c = \int_{\Omega} \left( \frac{1}{4} \varphi^2 (1 - \varphi)^2 + \frac{\varphi^2}{8} + \frac{\epsilon^2}{2} |\nabla \varphi|^2 \right. \\ \left. + \frac{\delta^2}{2} \left( \gamma_{11} (\varphi_{11}^2 + \varphi_{22}^2) + 4\gamma_{44} \varphi_{12}^2 + \gamma_{12} (\varphi_{11} + \varphi_{22})^2 \right) \right) d\Omega$$

$$E_e = \int_{\Omega} \left( \frac{\varphi^2}{8} + \frac{\delta^2}{2} \gamma_{12} (\varphi_{11}^2 + \varphi_{22}^2) \right) d\Omega$$

$$\gamma_{11}, \gamma_{44}, \gamma_{12} > 0$$



# Numerical Results

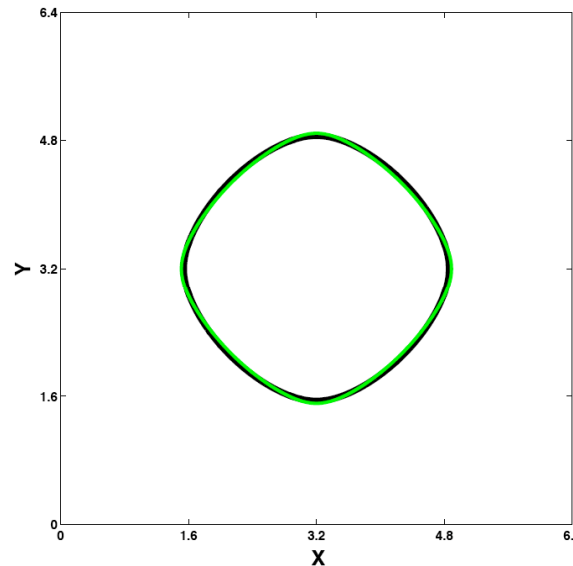
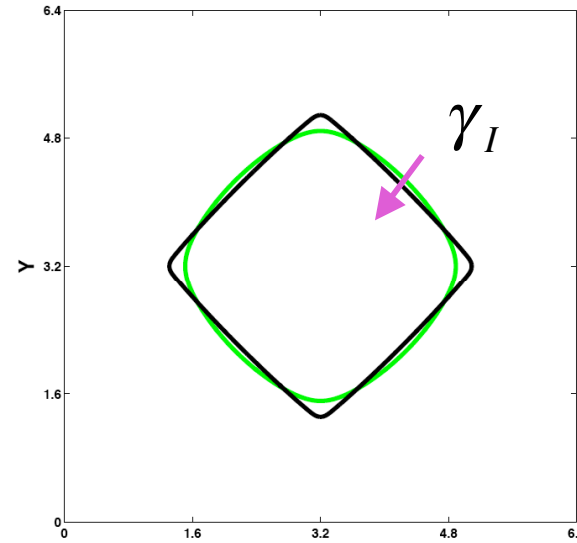
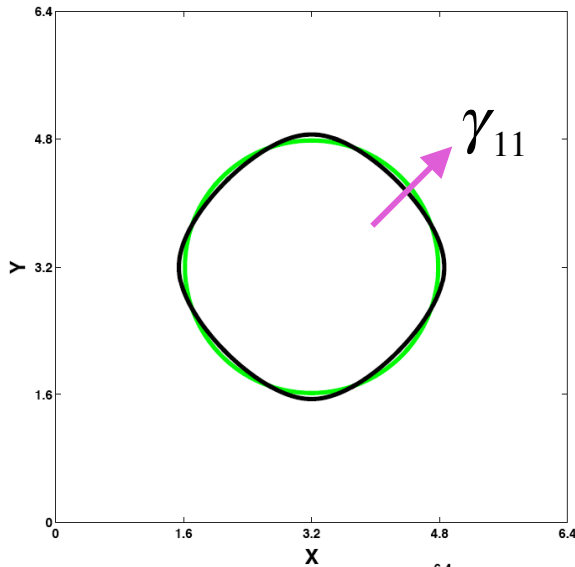
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Are there so many  
Coefficients?



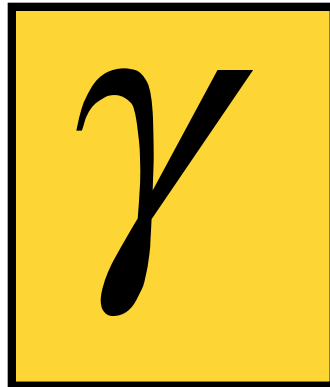


# Effect of Coefficients



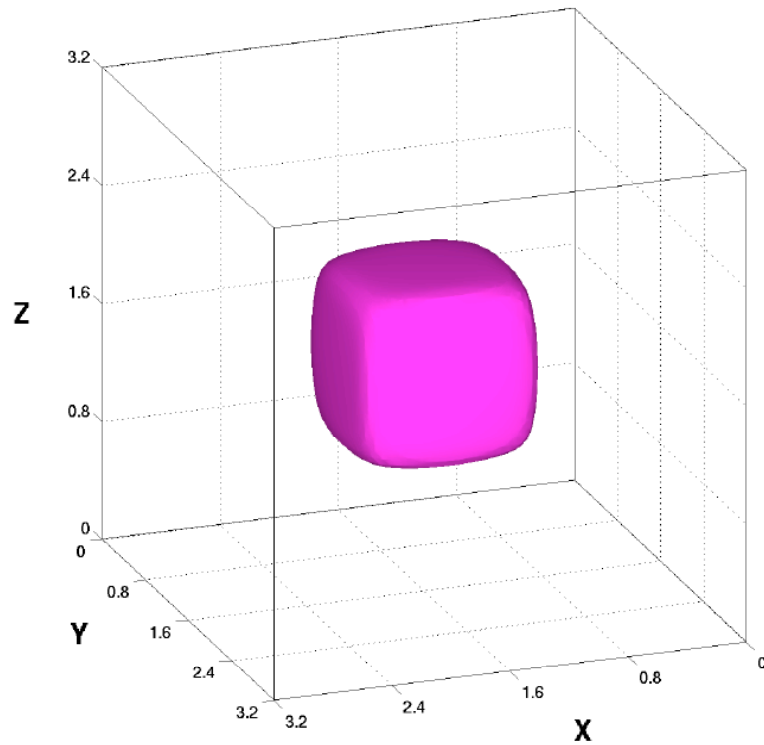
$$\begin{aligned}\delta &= 0.1 \\ \epsilon &= 0.001 \\ h &= 0.1 \\ s &= 0.001\end{aligned}$$

$$R_\gamma = \gamma_I / \gamma_{11}$$
$$\gamma_I = 2(\gamma_{12} + 2\gamma_{44} - \gamma_{11})$$

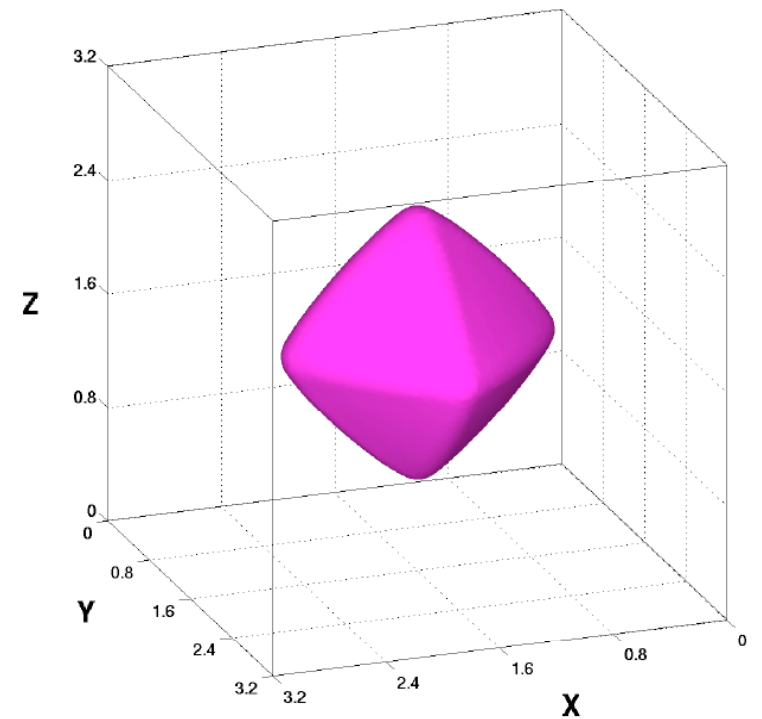




# Numerical Results in 3D



(a)  $\gamma_m = -1.4$

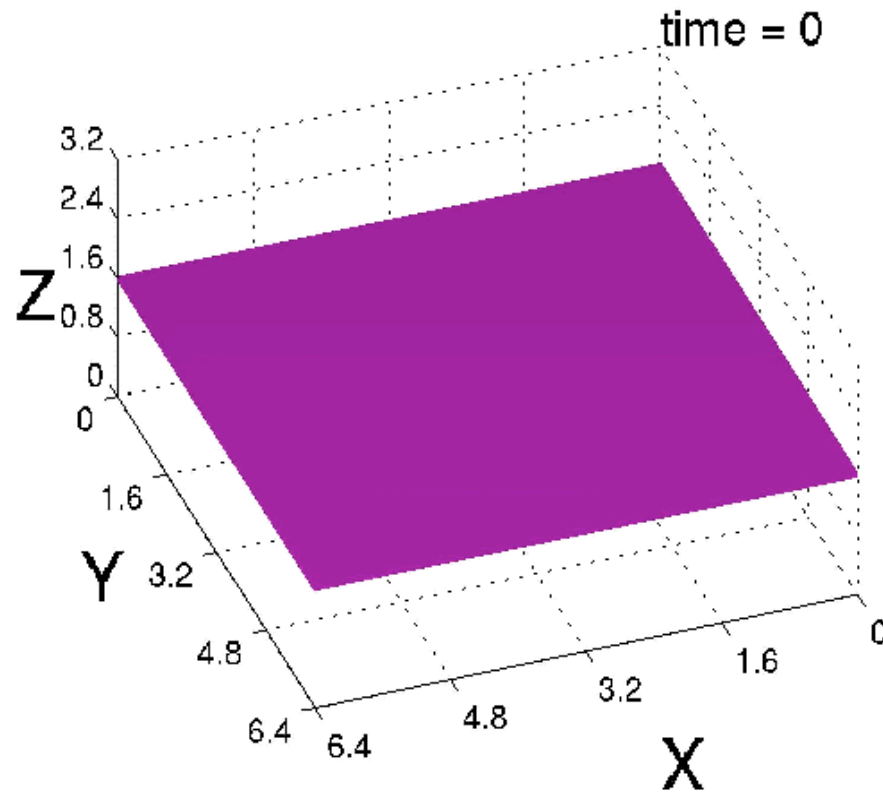
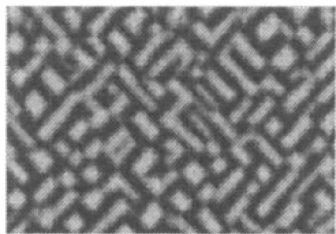
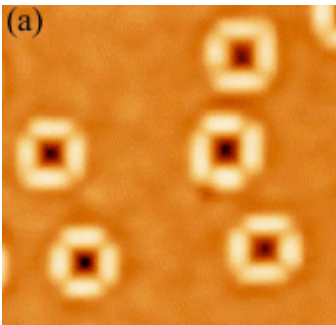


(b)  $\gamma_m = 1.4$



# 3D Evolution for flat Interface

$\{105\} \langle 100 \rangle$



$$M = 1$$

$$\gamma_{11} = 1$$

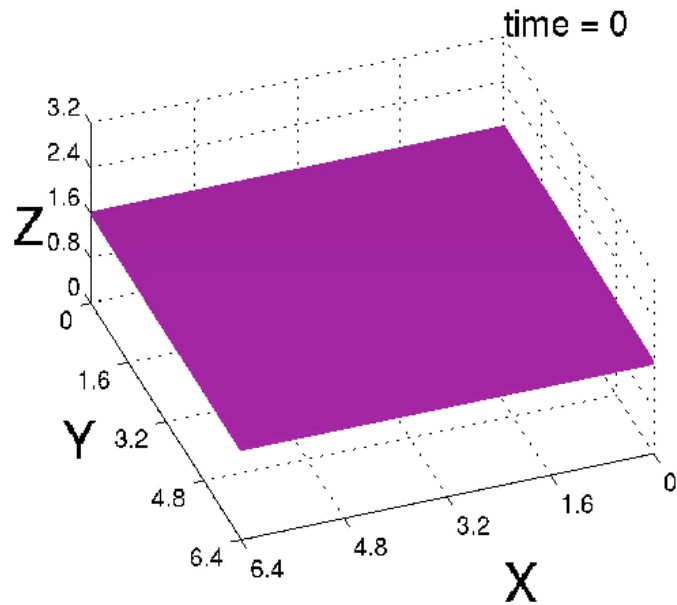
$$\gamma_m = 1.4$$

$\{111\}$

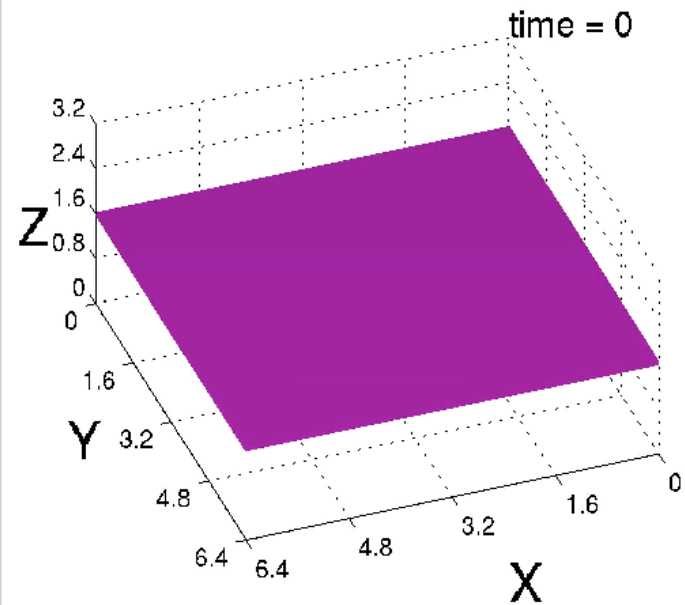
$\langle 110 \rangle$



# Effect of Mobility



$$M = 50$$

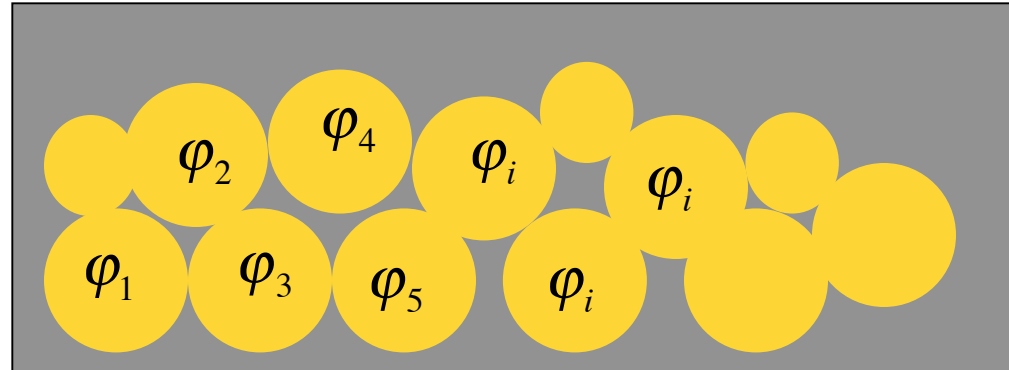


$$M = 1$$



# Sintering

Vapor



$$\sum \varphi_i = cte$$

Substrate





**Thank You**